

# On parametrized linear systems, moments, eigenvalues, gradients, and Krylov methods

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WSC Spring Meeting — Antwerp

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Collaborators:

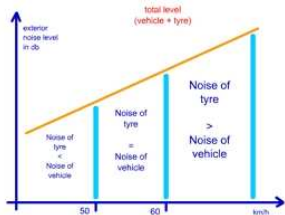
- Zhaojun Bai
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# Outline

- 1 Motivation
- 2 Overview of methods
  - Modal truncation
  - Vector-Padé approximation
  - Frequency sweeping
  - Input/output MOR
- 3 Lanczos method
- 4 Nonlinear frequency dependence
- 5 Multiple right-hand sides
- 6 Gradients
- 7 Conclusions

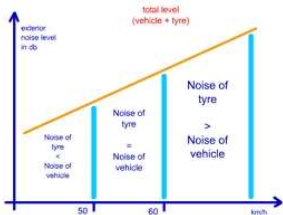
# Examples of vibrating systems

- Car tyres



# Examples of vibrating systems

## • Car tyres



## • Windscreens



- ▶ Structural damping
- ▶ Choice of connection (glue) to the car

# Examples of vibrating systems

- Planes



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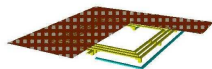


- Bridge vibrating under footsteps and Thames wind



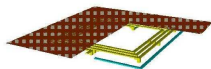
# Examples of vibrating systems

- Maxwell-equation – electrical circuits

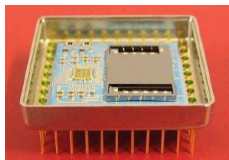


# Examples of vibrating systems

- Maxwell-equation – electrical circuits



- micro-gyroscope for navigation systems



# Fourier analysis of finite element model

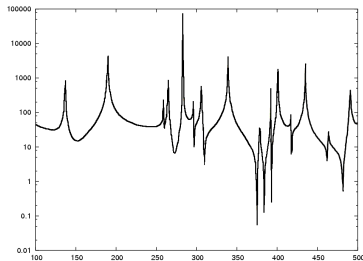
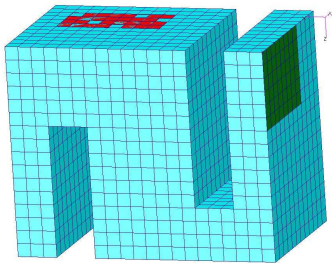


$$(K + i\omega C - \omega^2 M)\tilde{x} = \tilde{f}$$

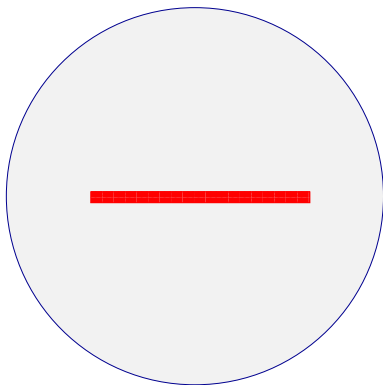
$f$  and  $x$  : vectors of length  $n$

$K$ ,  $C$  and  $M$  :  $n \times n$  sparse matrices. In real applications  $n$  varies from  $10^3$  to over  $10^6$ .

- $\tilde{x}$  is called the frequency response function.
- Compute  $x$  for  $\omega = \omega_1, \dots, \omega_p \in \Omega = [\omega_{\min}, \omega_{\max}]$ .



# Acoustic industrial applications : vibro-acoustics



- vibrating structure (modeled by structural **modes**)
- acoustic domain (**finite elements**)
- acoustic radiation towards infinity (infinite elements)
- structure is modeled by 'modes' (eigen functions)

# Traditional frequency response computation

1. For  $\omega = \omega_1, \dots, \omega_p$ 
  - 1.1. Solve the linear system  $(K + i\omega C - \omega^2 M)x = f$  for  $x$
  
- For each frequency, a large system of algebraic equations needs to be solved.  
This requires a linear solver for a large sparse matrix.
  - ▶ For a direct solver (based on LU factorization):
  - ▶ a sparse matrix factorization  $LU = K - \omega^2 M + i\omega C$  (expensive)
  - ▶ and a backward solve  $LUx = f$  (relatively cheap).

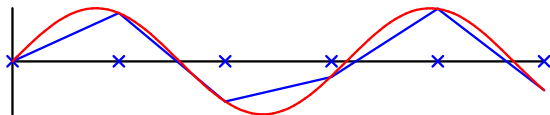
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The goal is to reduce the number of matrix factorizations.

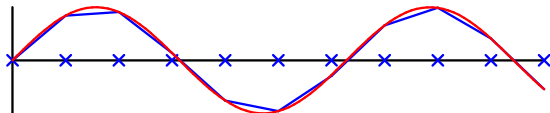
# Linear system solvers

- Discretization error depends on largest frequency: larger frequency means finer mesh



# Linear system solvers

- Discretization error depends on largest frequency: larger frequency means finer mesh



- Direct linear system solver: up to 1M dofs: no problem  
For a complex valued system of 3D volume discretization with 100,000 dofs, direct method solution time is of the order of 10 seconds.
- Iterative linear system solver
  - ▶ The last ten years effective preconditioners for the Helmholtz equation have been developed. [Erlangga, Vuik & Oosterlee, 2004, 2006], [van Gijzen, Erlangga, Vuik, 2007], [M. & 2008], [Vanroose & co]
  - ▶ Iterative methods can be seen as 'validation' of model
- AMLS [Bennighof]: automated level substructuring

# Overview of methods

Consider

$$(K - \omega^2 M)x = f$$

with

- $K$  and  $M$  large sparse, real symmetric matrices
- $M$  positive definite
- $f$  independent of  $\omega$ : typically point loads

Three basic methods:

- Modal truncation
- Padé approximation
- Mixed direct iterative procedure (fast frequency sweeping)

# Modal truncation

- Consider the eigendecomposition

$$Ku_j = \lambda_j Mu_j$$

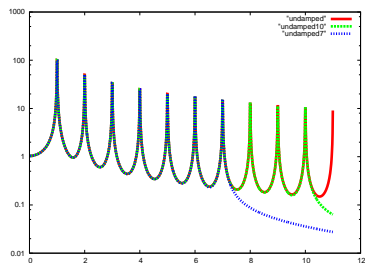
- The solution of  $(K - \omega^2 M)x = f$  is

$$x = \sum_{j=1}^n u_j \frac{u_j^T f}{\lambda_j - \omega^2}$$

- Rational function with poles  $\lambda_j$ .

## Modal superposition, cont.

$$x = \sum_{j=1}^n u_j \frac{u_j^T f}{\lambda_j - \omega^2} \approx \sum_{j=1}^k u_j \frac{u_j^T f}{\lambda_j - \omega^2}$$



# Vector-Padé approximation

Approximation of  $x = (K - \alpha M)^{-1}f$  by

$$\tilde{x} = \frac{x_0 + \alpha x_1 + \cdots + \alpha^{k-1} x_{k-1}}{(\alpha - \lambda_1) \cdots (\alpha - \lambda_k)}$$

This is a rational function with  $k$  poles.

Determine the coefficients so that

- the first  $k$  derivatives in  $\sigma$  match

# Frequency sweeping

For each  $\omega$  precondition

$$(K - \omega^2 M)x = f$$

into

$$(K - \sigma M)^{-1}(K - \omega^2 M)x = (K - \sigma M)^{-1}f$$

and solve by an iterative method.

- Use linear system solver for applying  $(K - \sigma M)^{-1}$
- For the AMLS method,  $K - \sigma M$  is a diagonal matrix.

# Input-output system

- SISO

$$\begin{aligned}(K - \omega^2 M)x &= b \\ y &= d^T x\end{aligned}$$

- Compute  $y$  accurately and fast
- Use MOR as fast solver
- Often many outputs (100's or 1000's)
- Twosided methods (MOR) are not often used in this case

# Summary

- Modal truncation:

$$\tilde{x} = \sum_{j=1}^k u_j \frac{u_j^T f}{\lambda_j - \alpha}$$

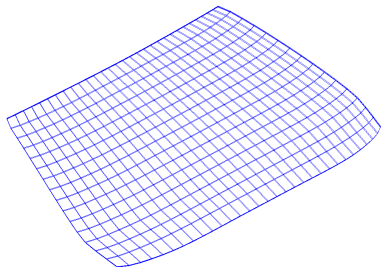
- Padé approximation:

$$\tilde{x} = \frac{x_0 + \alpha x_1 + \dots + \alpha^{k-1} x_{k-1}}{(\alpha - \mu_1) \cdots (\alpha - \mu_k)}$$

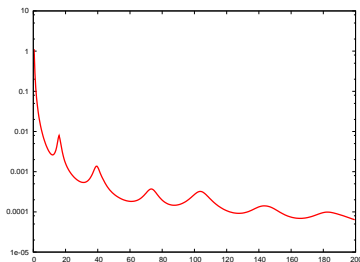
- Frequency sweeping  
Solve  $(M - \omega^2 M)x = f$  by an iterative method
- MOR: find reduced model for linear system

$$\begin{aligned}(K - \omega^2 M)x &= b \\ y &= d^T x\end{aligned}$$

# Numerical example: BMW Windscreen



- Glaverbel-BMW windscreen with 10% structural damping
- Direct method : 2653 seconds
- Lanczos method : 14 seconds



# Notation

- Define  $\alpha = \omega^2$
- $A = (K - \sigma M)^{-1}M$  and  $b = (K - \sigma M)^{-1}f$
- Assume  $\sigma = 0$  and

then we solve

$$(K - \alpha M)x = f$$

or

$$\begin{aligned}(K - \sigma)^{-1}(K - \alpha M)x &= (K - \sigma)^{-1}f \\ (I - \alpha A)x &= b\end{aligned}$$

Eigenvalue problem:

$$Ku_j = \lambda_j Mu_j$$

Assume  $A$  symmetric.

# Lanczos method

- Krylov space:  $\text{span}\{b, Ab, \dots, A^{k-1}b\}$
- Lanczos method builds orthogonal basis  $V_k = [v_1, \dots, v_k]$ .

$$\text{Range}(V_k) = \text{span}\{b, Ab, \dots, A^{k-1}b\}$$

- and a tridiagonal matrix  $T_k = V_k^T A V_k$
- major cost:  $k$  matrix vector products with  $A$  :  $w = Av$
- small cost when  $k$  is small
- Also called Ritz vector technique (mechanical engineering)

# Lanczos method

Transform a large size matrix into a small size matrix

The diagram illustrates the Lanczos method transformation. On the left, a small square matrix  $T_k$  is shown with a dashed border and three parallel diagonal lines. This is followed by an equals sign. To the right of the equals sign is a solid rectangular box representing  $V_k^T$ . This is followed by a large dashed square representing the matrix  $A$ . Finally, there is a solid vertical rectangular box representing  $V_k$ .

$$T_k = V_k^T A V_k$$

# Shift-invariance property

- Krylov spaces

$$\{v, Av, A^2v, \dots\}$$

and

$$\{v, (I - \alpha A)v, (I - \alpha A)^2v, \dots\}$$

are equal, since  $(I - \alpha A)v = v - \alpha Av$

- Applying the Lanczos method to  $A$ , applies it for free to  $A + \alpha I$  for all  $\alpha$ .

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- Applying the Lanczos method to  $A$ , applies it for free to  $A + \alpha I$  for all  $\alpha$ .
- As, a consequence,

$$\begin{aligned}V_k^T AV_k &= T_k \\V_k^T (I - \alpha A)V_k &= I - \alpha T_k\end{aligned}$$

- Therefore, no need to build Krylov space for different values of  $\alpha$

# Shifted or parameterized linear systems

- Analyzed in the context of model reduction methods (Connection with rational approximation)  
[Gallivan, Grimme, Van Dooren 1994], [Feldman, Freund 1995], [Gallivan, Grimme, Van Dooren 1996], [Grimme, Sorensen, Van Dooren 1996], [Ruhe & Skoogh 1998], [Bai & Freund 2000], [Bai & Freund 2001] [Bai & Su 2006]
- in the context of parameterized linear systems  
[Freund 1993], [Frommer & Glässner, 1993], [Simoncini & Gallopoulos 1998], [Simoncini, 1999, 2010], [Simoncini & Perotti 2002], [M. 2003], [Edema, Vuik 2008], [M. 2008], [M. & Bai, 2010]

# Undamped vibration problem

- When  $A = K^{-1}M$ ,  $A$  is non-symmetric.
- However,  $x^T MAy = y^T MAx$  for all  $x, y$ . So,  $A$  is self-adjoint with the  $M$  inner product
- Use the Lanczos method with  $M$  orthogonalization:

$$V_k^T M V_k = I$$

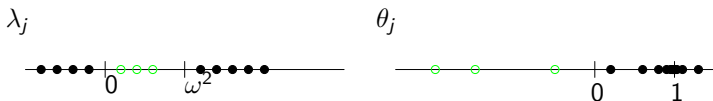
- Matrix vector products with  $A$ :
  - ▶ One matrix factorization of  $K = LDL^T$
  - ▶  $k$  solves of the form  $LDL^T w = Mv$

## Iterative solver connection

- Lanczos method (Conjugate gradients) is iterative linear system solver for

$$(I - \alpha A)x = b$$

- Let  $A = K^{-1}M$
- Let  $Ku_j = \lambda_j Mu_j$
- Eigenvalues of  $K^{-1}(K - \omega^2 M)$  are  $\theta_j = \frac{\lambda_j - \omega^2}{\lambda_j}$
- Fast convergence when most eigenvalues are clustered around one:
  - ▶  $\omega$  close to 0



- When there are no eigenvalues  $\lambda$  between 0 and  $\omega^2$ , then we have a positive definite linear system

# MINRES versus Lanczos

- Lanczos:

$$\tilde{x} = \sum \frac{y_j}{\alpha - \mu_j}$$

- ▶ Vertical asymptotes

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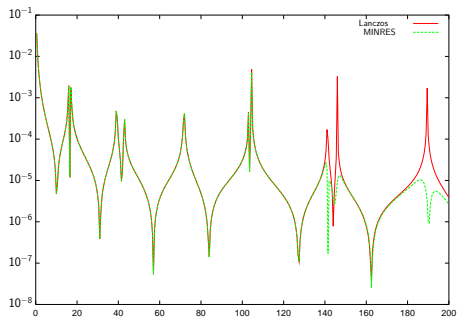
- ▶ Vertical asymptotes

- MINRES:

$$\tilde{x} = \sum \frac{y_j(\alpha)}{\alpha - \mu_j(\alpha)}$$

- ▶ Denominator is never zero
- ▶ No vertical asymptotes

# Example



## Eigenvalue and Padé connection

- Lanczos method produces  $k$  eigenvalue estimates: eigenvalues of  $T_k$   
We can show that the Lanczos method computes

$$\tilde{x} = \sum_{j=1}^k \tilde{u}_j \frac{\tilde{w}_j^T f}{\lambda_j - \alpha}$$

where  $\tilde{u}_j$  is a Ritz vector (i.e. approximate eigenvector).

- ▶ There are  $k$  terms, so we can only compute  $k$  vertical asymptotes in the function
- ▶ The number of eigenvalues in the frequency range should be smaller than  $k$ .

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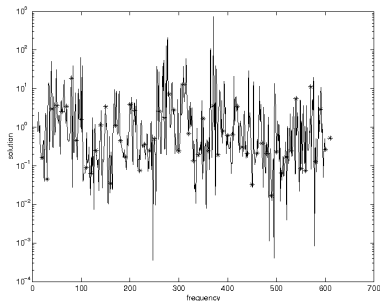
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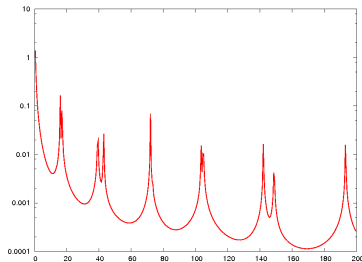
- ▶ There are  $k$  terms, so we can only compute  $k$  vertical asymptotes in the function
  - ▶ The number of eigenvalues in the frequency range should be smaller than  $k$ .
- Padé connection:  $\tilde{x}$  is a rational approximation with

$$x^{(j)}(0) = \tilde{x}^{(j)}(0) \quad \text{for } j = 0, \dots, k - 1$$

# Eigenvalue connection: example



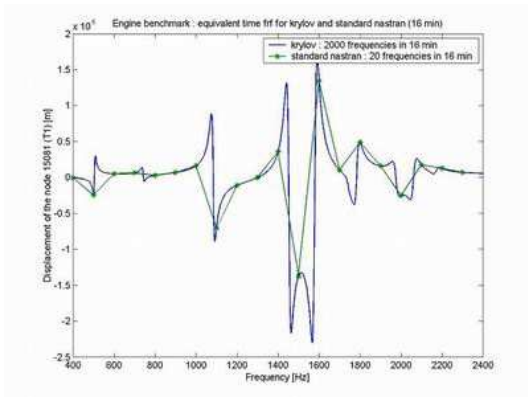
Hard problem: more than 10,000 eigenvalues



Easy problem: less than 20 eigenvalues

# Industrial example with NASTRAN

- Traditional computation
  - ▶ For each frequency, perform factorization of  $K - \omega^2 M$  and solve
- Lanczos computation
  - ▶ One matrix factorization of  $K - \sigma M$  and solve
  - ▶  $k$  solves.



# Nonlinear frequency dependence

$$(K + i\omega C - \omega^2 M)x = f$$

- 'Linearization':

- ▶ Define matrices  $A$  and  $B$

$$A = \begin{bmatrix} K & \\ & I \end{bmatrix} \quad B = \begin{bmatrix} iC & -M \\ I & \end{bmatrix}$$

so that

$$(A - \omega B) \begin{pmatrix} x \\ \omega x \end{pmatrix} = \begin{pmatrix} f \\ 0 \end{pmatrix}$$

This is called a linearization, a similar trick as the solution of second order ODE's.

# Linearizations

- Linearizations have been studied for the solution of the quadratic eigenvalue problem

$$(K + \lambda C + \lambda^2 M)u = 0$$

[Gohberg, Lancaster, Rodman, 1982] [Tisseur, M. 2001]  
[Mackey, Mackey, Mehl, Mehrmann, 2006]

- Methods based on Companion 'linearization'
- Higher order polynomials

$$(A_0 + \omega A_1 + \dots + A_p \omega^p)x = f$$

Transform to

$$\left( \begin{bmatrix} A_0 & & & & \\ & -I & & & \\ & & \ddots & & \\ & & & -I & \end{bmatrix} + \omega \begin{bmatrix} A_1 & A_2 & \dots & A_p \\ I & 0 & & \\ & \ddots & \ddots & \\ & & I & 0 \end{bmatrix} \right) \begin{pmatrix} x \\ \omega x \\ \vdots \\ \omega^{p-1}x \end{pmatrix} = \begin{pmatrix} f \\ 0 \\ \vdots \\ 0 \end{pmatrix}$$

# Methods

- [Parlett & Chen 1990] Pseudo Lanczos method (pretends  $B$  is positive definite)
- [Simoncini & al, 2005] similar
- [Freund, 2005]: analysis of Krylov spaces
- [Bai & Su, 2005] SOAR: based on Arnoldi's method
- [M. 2008] Q-Arnoldi: based on Arnoldi's method (for eigenvalue problems)
- [Amiraslani, Corless, Lancaster, 2009] Other polynomials than powers of  $\omega$ .
- [Jarlebring, M., Michiels 2010] Infinite-Arnoldi: based on Arnoldi's method (for delay eigenvalue problem)

## Multiple right-hand sides

$$(K - \omega^2 M)[x_1, \dots, x_s] = [f_1, \dots, f_s]$$

for  $\omega \in \Omega = [\omega_{\min}, \omega_{\max}]$ .

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Methods:

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  - ▶ Low memory cost
  - ▶ The cost is proportional to  $s$

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- Use block-Lanczos method for each all  $f_j$  together
  - ▶ Fast method
  - ▶ High memory cost

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- Recycling Ritz vectors in Krylov methods [Giraud, Ruiz & Touhami, 2006] [Kilmer & de Sturler 2006] [Darnell, Morgan, Wilcox 2007] [Stathopoulos & Orginos, 2009][M. & Bai, 2010]

# Recycling

- Compute the FRF for the first right-hand side
- Extract eigenvalues / eigenvectors
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$$\hat{x} = \sum_{j=1}^k \hat{u}_j \frac{\hat{u}_j^T f}{\hat{\lambda}_j - \omega^2}$$

- ★ First  $k$  moments of  $\hat{x}$  and  $x$  match.

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- ★ First  $k$  moments of  $\hat{x}$  and  $x$  match.
- ▶ With reuse of eigenvalues:

$$\hat{x} = \sum_{j=1}^p u_j \frac{u_j^T f}{\lambda_j - \omega^2} + \sum_{j=p+1}^k \hat{u}_j \frac{\hat{u}_j^T f}{\hat{\lambda}_j - \omega^2}$$

- ★ First  $k - p$  moments of  $\hat{x}$  and  $x$  match.
- ★ Interpolation in the  $p$  deflated eigenvalues.

# Frequency sweeping with modal acceleration

The solution of

$$(I - \omega^2 A)x = b \quad (1)$$

for  $\omega \in \Omega$  is split into two parts.

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- Let  $U_p = [u_1, \dots, u_p]$  be the eigenvectors corresponding to the eigenvalues in  $\Omega^2$ .
- Compute

$$x_p = \sum_{j=1}^p u_j \frac{u_j^T f}{\lambda_j - \omega^2}$$

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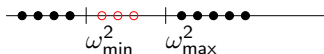
- Solve (1) iteratively using starting vector  $x_p$ , i.e.  $x = x_p + y$  with  $y$  the solution of

$$\begin{aligned}(I - \omega^2 A)y &= b - (I - \omega^2 A)x_p \\ &= (I - U_p U_p^T M)b\end{aligned}$$

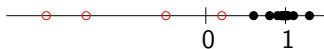
# Modal acceleration

- We can prove that eigenvalues in the frequency range are computed to machine precision
- As a result, the right-hand side has 'no' components in the associated eigenvalues
- This significantly improves the condition number

Eigenvalues of  $Kx = \lambda Mx$



Eigenvalues of  $A$



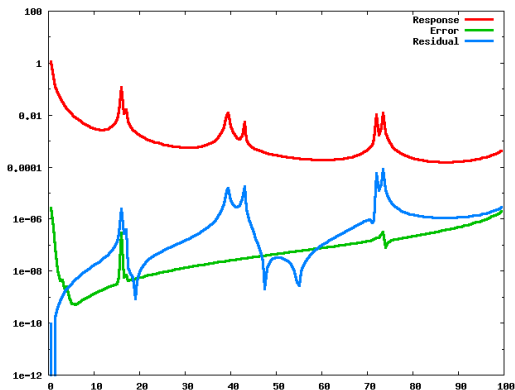
- ▶ Most eigenvalues of  $A$  lie near one.
- ▶ The number of required iterations is the number of isolated eigenvalues of  $A$  away from one.
- ▶ Convergence for all  $\omega^2 \in \Omega^2$  requires the number of iterations,  $k$ , to be at least the number of eigenvalues in  $\Omega^2$ .
- ▶ Remove the red eigenvalues: positive definite matrix, and small condition number

# Windscreen

- Glaverbel-BMW windscreen
- grid : 3 layers of  $60 \times 30$  HEX08 elements ( $n = 22,692$ )
- $\Omega = [0, 100]$
- First run:
  - ▶ unit point force at one of the corners
  - ▶ Use Lanczos method with  $k = 20$  vectors.
  - ▶ We keep the Ritz values in  $[0, 2 \times 100^2]$  :  $p = 14$

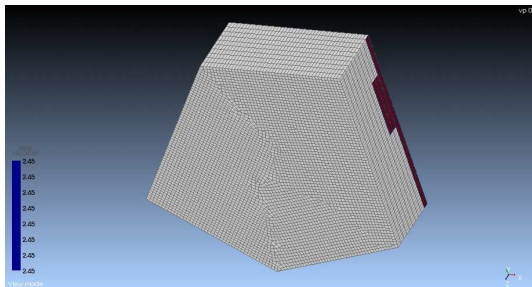
# Windscreen

- Second run with other right-hand side
  - ▶ Perform 6 additional Lanczos steps



- ▶ The largest condition number of linear system is 1.9813.
- ▶ Six iterations reduce the error by  $2 \cdot 10^{-5}$ .

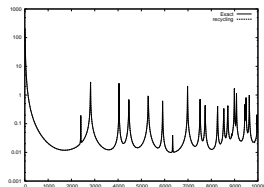
# Acoustic cavity



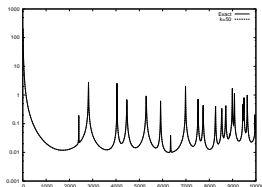
- $n = 48,158$
- Frequency range :  $[0, 10000]$
- 202 right-hand sides
- matrix factorization: 8 seconds
- Lanczos method with 40 vectors: 6 seconds

## Acoustic cavity (cont.)

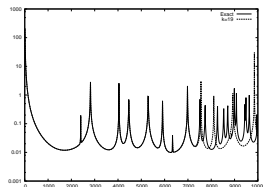
- 2nd right-hand side: keep the 31 Ritz values in  $[0, 2 \times 10.000^2]$ .
- 9 additional Lanczos iterations recycling 31 Ritz vectors: 2 seconds



With recycling

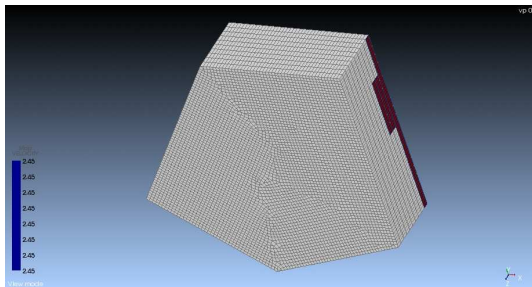


Lanczos  $k = 50$



Lanczos  $k = 19$

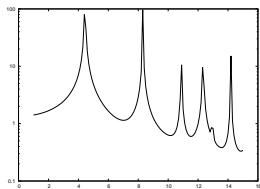
# Acoustic cavity



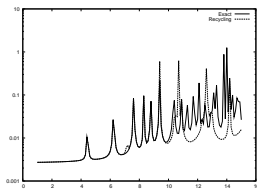
- $n = 140,228$
- Frequency range :  $[0, 10000]$
- 202 right-hand sides
- matrix factorization: 13 seconds
- Lanczos method with 50 vectors: 15 seconds
- Recycling 36 vectors: only 4 seconds
- For 201 right-hand sides: 800 instead of 3000 seconds.

# Multiple eigenvalues

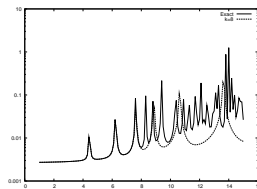
- 3D Laplacian on a cube.
- 30 Lanczos iterations with first right-hand side
- Recycle 22 Ritz pairs
- Run 8 iterations with the second right-hand side



Lanczos for  $f_1$



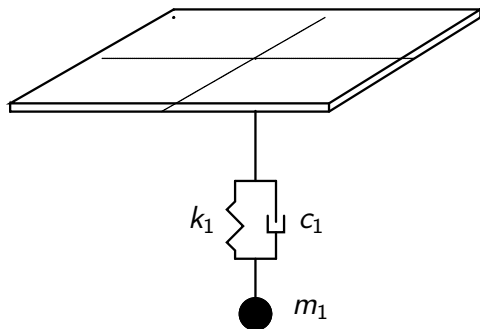
Recycling for  $f_2$



Lanczos  $k = 8$  for  $f_2$

# Gradient computation

- Determination of optimal parameters of a vibrating system
- Example: optimal parameters for a damper of a floor in a building near a noisy road



# Optimization problem

- Parametrized linear system:

$$\begin{cases} (K(p) + i\omega C(p) - \omega^2 M(p))x = f \\ y = d^T x \end{cases}$$

- Find parameters  $p$  so that
  - ▶  $\|y\|_2 = \int_0^{\omega_{\max}} |y|^2 d\omega$  is minimal
  - ▶  $\|y\|_\infty = \sup_0^{\omega_{\max}} |y|^2$  is minimal
- This is, in general, a non-smooth optimization problem
- Expensive evaluation of  $y$  and the gradient
- Model order reduction is an important tool to reduce the computational cost
  - ▶ Both function value and gradient should be computed by the reduced model

# Gradient computation

- [Antoulas, Beattie, Gugercin 2010] [Yue, M. 2010] show interpolation properties on derivatives for two-sided MOR:

$$\begin{cases} (K(p) + i\omega C(p) - \omega^2 M(p))x & = f \\ y & = d^T x \end{cases}$$

- ▶  $Z(\omega) = K + i\omega - \omega^2 M$
  - ▶  $x = Z(\omega)^{-1} f$
  - ▶  $y = d^T x$
  - ▶  $\frac{\partial y}{\partial p} = (Z(\omega)^{-1} d)^T \frac{\partial Z(\omega)}{\partial p} Z(\omega)^{-1} f$
- $Z(\omega)^{-T} d$  and  $Z(\omega)^{-1} f$  are computed by two-sided Krylov methods

# Numerical example

- Floor with damper ( $n = 29800$ )
- Reduced model  $k = 25$
- Determine optimal parameters

	Direct method	Krylov
Matrix size	29800	25
Optimizer computed	(14007181, 42404)	(14007225, 42410)
Function value	134.5477989	134.5479496
CPU time	Several Days	3735s

# Conclusions

- Krylov methods usually work well for acoustic simulation
- Recycling Ritz vectors is a reliable and efficient method for the solution with multiple right-hand sides
- Parametrized models with many parameters are current challenges
- Solving parameterized linear systems with multiple right-hand sides can benefit from recycling Ritz vectors
- Does not work well when eigenvalues are multiple
- Also works for Rayleigh damping

# Bibliography

(Also: [www.cs.kuleuven.be/~karlm](http://www.cs.kuleuven.be/~karlm))



J. De Vlieger and K. Meerbergen.

Analysis and computation of eigenvalues of symmetric fuzzy matrices.  
In T. Simos, editor, *Proceedings of the ICNAAM09 Conference*, 2009.



K. Meerbergen.

The solution of parametrized symmetric linear systems.  
*SIAM J. Matrix Anal. Appl.*, 24(4):1038–1059, 2003.



K. Meerbergen.

Fast frequency response computation for Rayleigh damping.  
*International Journal of Numerical Methods in Engineering*, 73(1):96–106, 2008.



K. Meerbergen.

The Quadratic Arnoldi method for the solution of the quadratic eigenvalue problem.  
*SIAM J. Matrix Anal. and Applic.*, 30(4):1463–1482, 2008.



K. Meerbergen and Z. Bai.

The Lanczos method for parameterized symmetric linear systems with multiple right-hand sides.  
*SIAM J. Matrix Anal. and Applic.*, 31(4):1642–1662, 2010.



K. Meerbergen and J.P. Coyette.

Connection and comparison between frequency shift time integration and a spectral transformation preconditioner.  
*Numerical Linear Algebra with Applications*, 16:1–17, 2009.



F. Tisseur and K. Meerbergen.

The quadratic eigenvalue problem.  
*SIAM Review*, 43(2):235–286, 2001.